

# Improving the Detection Capability of Vertical and Horizontal Failures in Terrain Database Integrity Monitors

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# Introduction

- A Flight Safety Foundation Study revealed that 41% of all aircraft accidents involved Controlled Flight into Terrain (CFIT)
- CFIT means the aircraft runs into terrain (mountains, or land while flying low) even though the aircraft is under full control of the pilot
- Principal cause of CFIT is loss of spatial orientation during zero visibility conditions due to bad weather like rain, fog, snow or darkness



# Remedial Measures

## Government Programs

- NASA's Aviation Safety Program
  - » **Synthetic Vision Systems (SVS) Project**
- FAA's Safeflight21 Program
- NIMA's Ron Brown Airfield Initiative



# What Are Synthetic Vision Systems ?

- Advanced display technology containing information about aircraft state, guidance, navigation, surrounding terrain and traffic
- A computer generated (*synthetic*) image of the outside world as viewed “from the cockpit”
- Provides either a Heads-Up Display (HUD) or a Heads-Down Display (HDD)
- Clear view in all weather conditions at all times



# Source of Synthetic Vision Displays

- Digitally stored terrain heights known as Digital Elevation Models (DEMs) or Digital Terrain Elevation Databases (DTEDs)
- Similar to having a digital lookup table containing terrain heights
- Eg: DTED level 0,1,2, Jeppesen



# Why Terrain Database Integrity Monitoring ?

**Terrain Databases may have systematic faults due to:**

- Different sensor technologies used to generate the terrain databases
- Manual post – processing of collected data
- Flat earth approximation over relatively large areas

Use of Synthetic Vision Displays for functions other than their intended applications



# Errors Present in Terrain Databases

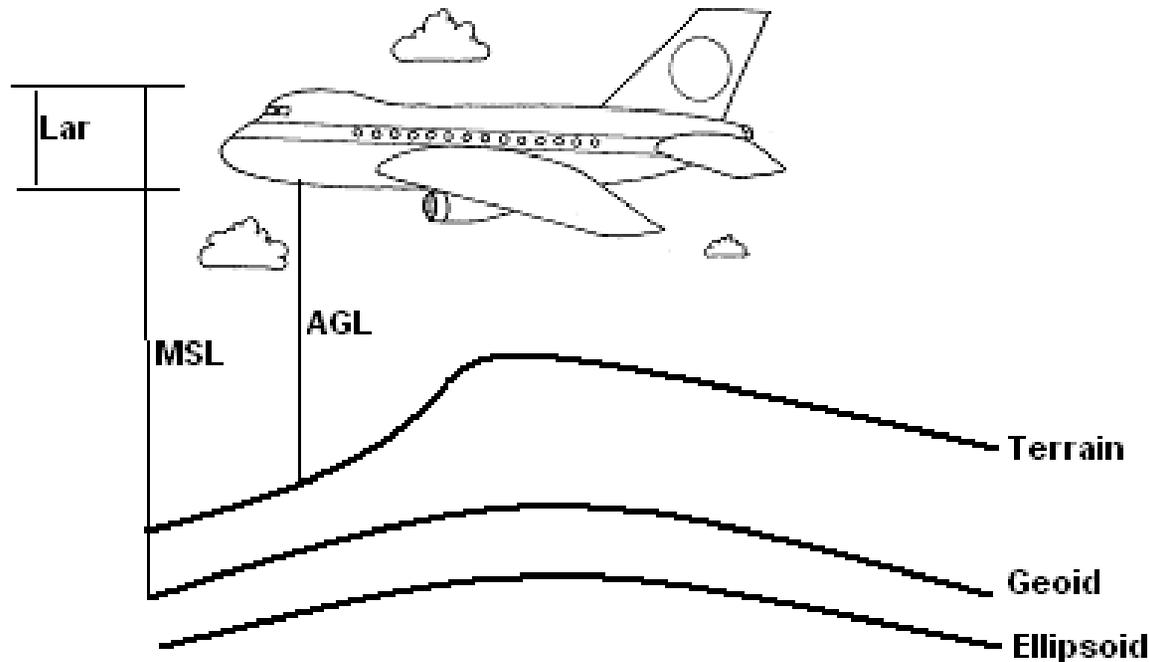
Errors in the form of:

- Bias – due to coordinate transformation mismatch
  - » Vertical domain
  - » Horizontal domain
- Ramps
  - » Vertical domain
  - » Horizontal domain
- Random Errors
  - » Distributed errors in Vertical Domain
  - » Circularly distributed errors in the Horizontal Domain



# Vertical Direction Integrity Monitor

Comparison of the DEM terrain profile with and independent terrain profile synthesized from a downward looking sensor such as a Radar Altimeter (RA) and GPS WAAS measurements\*



**Synthesized Height = MSL – AGL – Lar**

**DTED Height = elevation with respect to MSL**

\* Dr. Robert Gray's original Integrity Monitoring Concept

# Comparison Metrics

The metrics used to express agreement between the two terrain profiles are:

- Absolute Disparity:

$$p(t_i) = h_{\text{synt}}(t_i) - h_{\text{DTEd}}(t_i)$$

» Sensitive to bias errors

Mean Squared Difference (MSD) =

$$\frac{1}{N} \sum_{i=1}^N p^2(t_i)$$

- Successive Disparity:

$$s(t_i) = p(t_i) - p(t_{i-1})$$

» Sensitive to ramp errors

Mean Absolute Difference (MAD) =

$$\frac{1}{N-1} \sum_{i=2}^N s^2(t_i)$$

- Cross Correlation (XCORR)

These metrics are random variables and would require test statistics for their characterization



# Formulation of Hypotheses

- Null or Fault – Free Hypothesis:
  - » Nominal error performance: just normal random errors

$$H_0 : p_0 \sim N(0, \sigma_p^2)$$

Normally distributed errors with zero mean (no bias) and known convolved variance of errors  $\sigma_p^2$

- Alternative or Faulted Hypothesis:
  - » Off-nominal behavior: failure, which means the presence of bias and ramp errors

$$H_1 : p_1 \sim N(\mu_B, \sigma_p^2)$$

Normally distributed errors with mean  $\mu_B$  (bias) and variance  $\sigma_p^2$



# So, Why Do We Need a Statistical Framework?

The distribution of the metrics used to perform hypothesis testing which is nominally due to the inherent presence of:

- Measurement noise on sensors used for comparison (RA, GPS positions)
- Vertical and Horizontal Error probability specification of the DEM
- Random errors on the DEM
- Ground Cover (Vegetation)



# The 'T' Statistic for Hypothesis Testing

If the MSE is scaled by the variance of the noise on the absolute disparities under nominal conditions, it gives rise to a test statistic,  $T$ , which is a measure of consistency between the two terrain profiles.

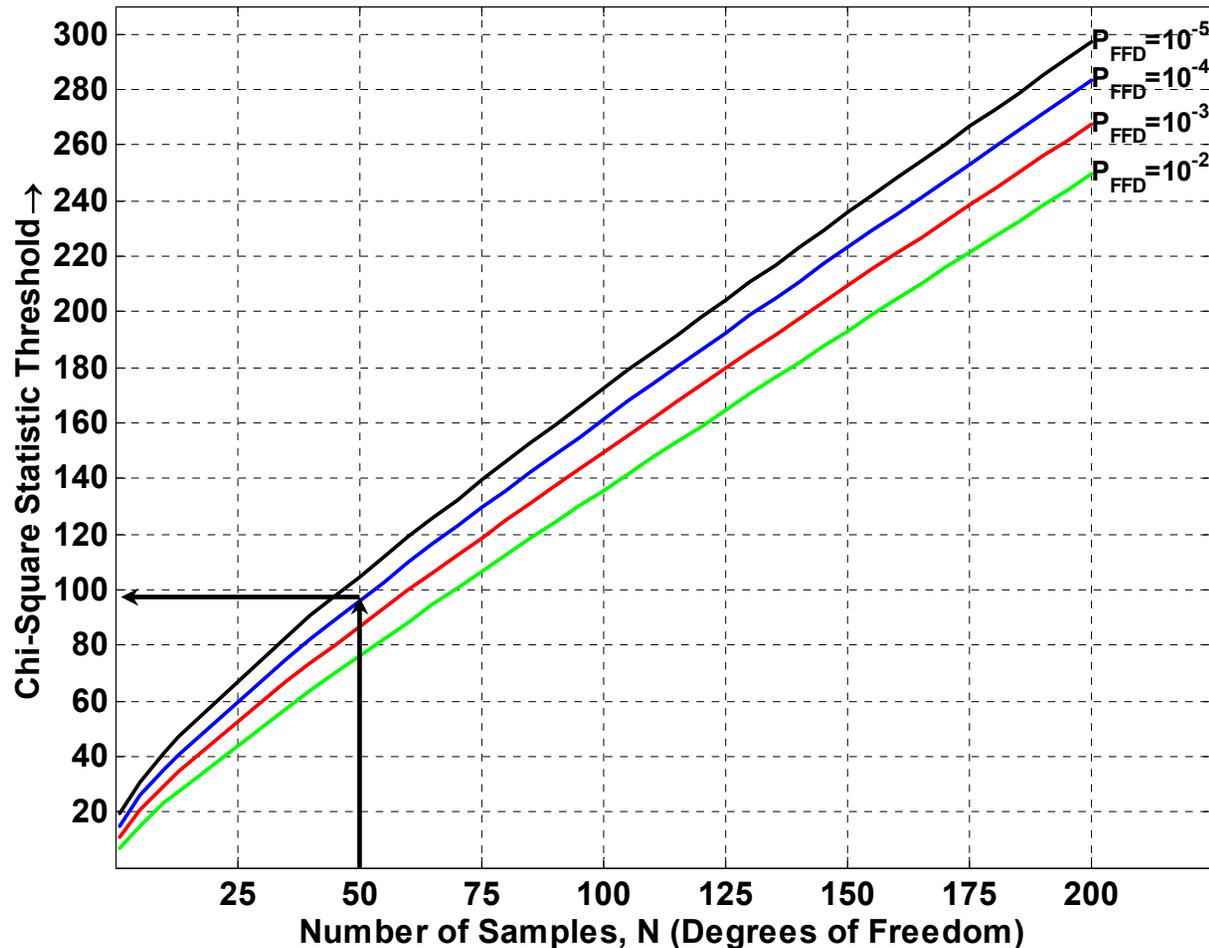
$$T = \frac{1}{\sigma_p^2} \sum_{i=1}^N p^2(t_i)$$

**This is a standard Chi – Squared statistic, but what should be its Threshold ?**



# How Do We Know the Threshold for T ?

The threshold value for T is determined by the probability of Fault – Free Detection,  $P_{FFD}$  and the number of degrees of freedom, N



# Horizontal Integrity Monitor

## Multiple Path DLIM

- Look for multiple flight paths parallel to the nominal over a search grid and compute the chi – squared test statistic as a measure of conformity between the two terrain profiles.

$$T(m, n) = \frac{1}{\sigma^2} \sum_{i=1}^N (h_{SYNT}(t_i) - h_{DTED}(x, y))^2$$

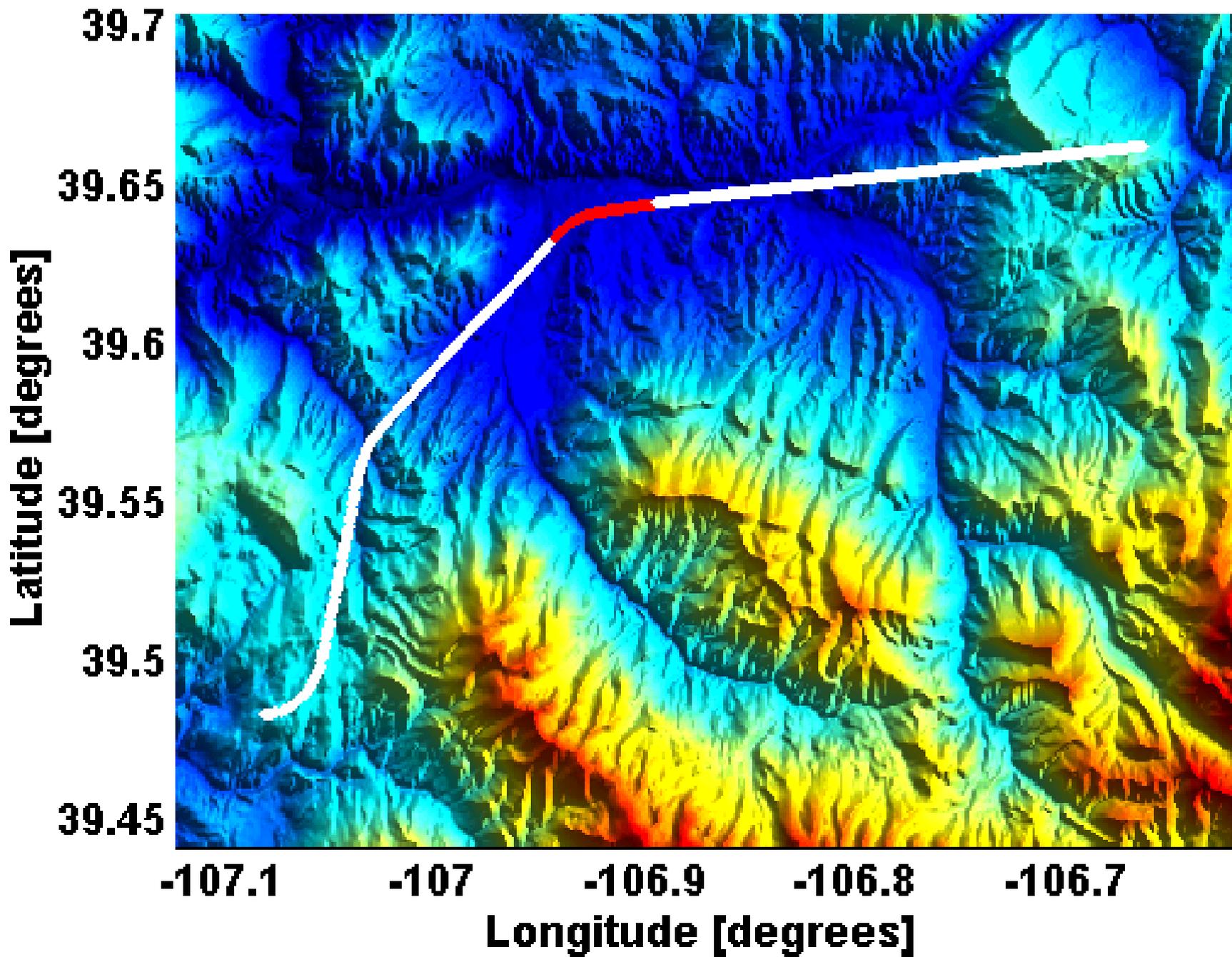
Where,  $x = lat(t_i) + lat\_offset_m$  for  $m = -P$  to  $P$

$y = lon(t_i) + lon\_offset_n$  for  $n = -P$  to  $P$

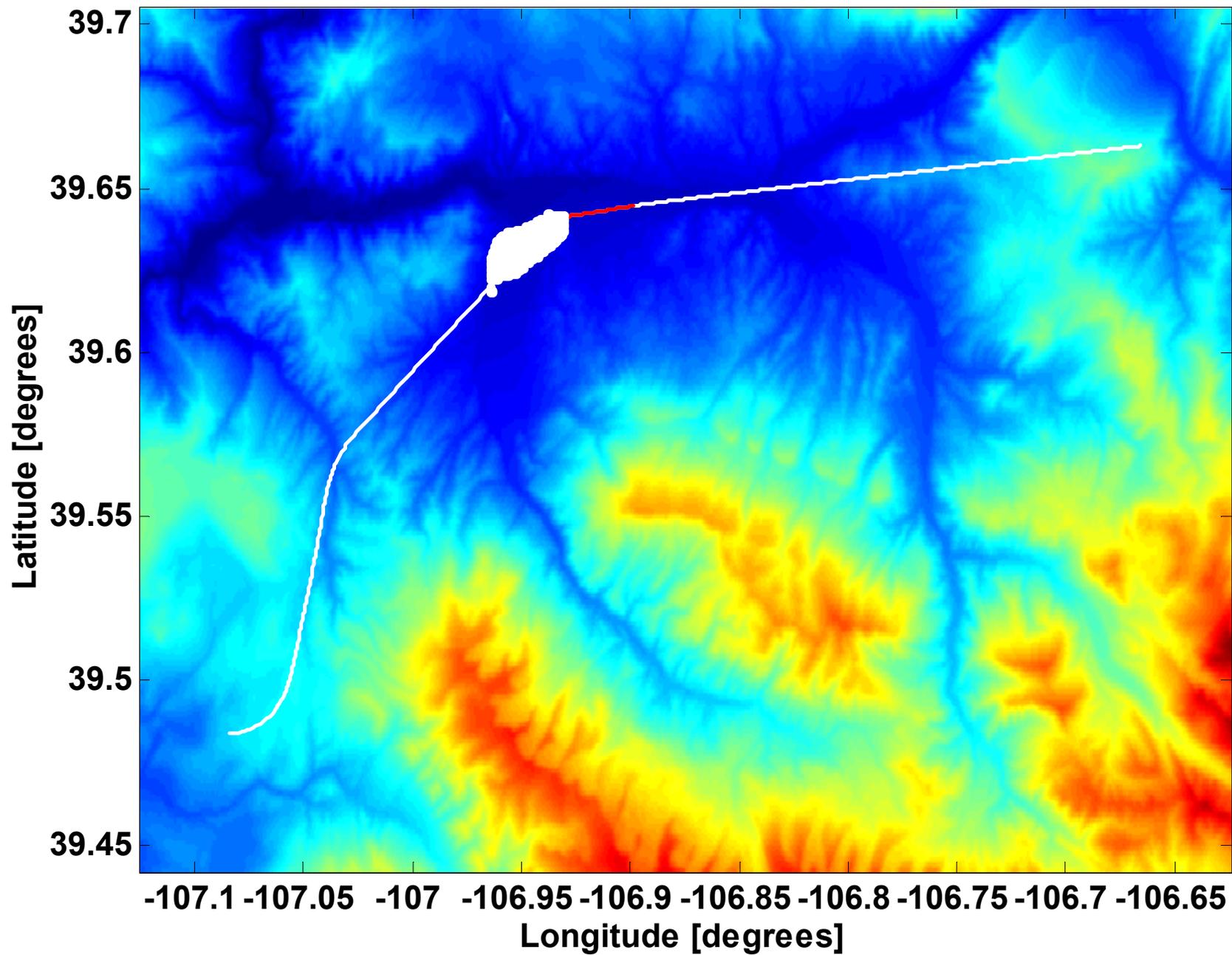
- Determine if one or more of these translated positions are the actual positions on the DTED corresponding to the DGPS position



# Terrain Elevation & Flight Path Plot



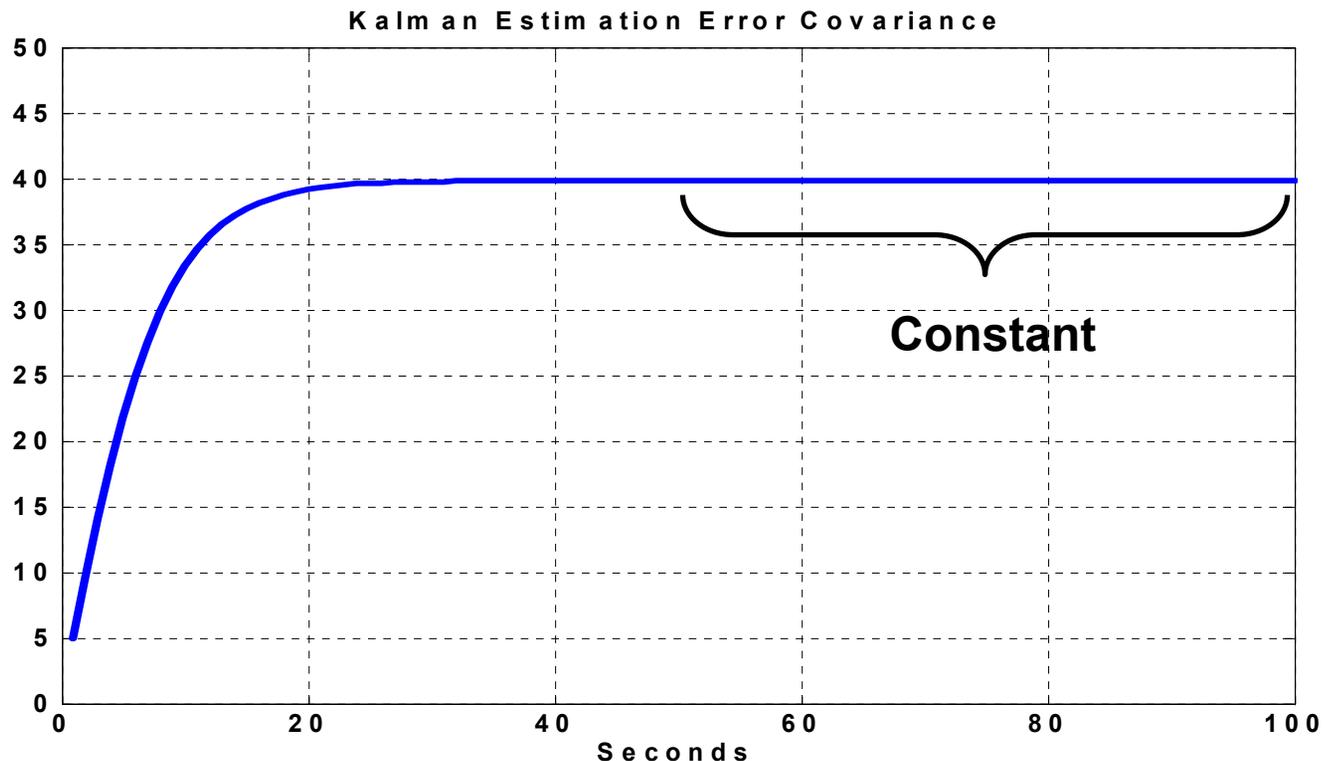
# Terrain Elevation & Probable Horizontal Displacement



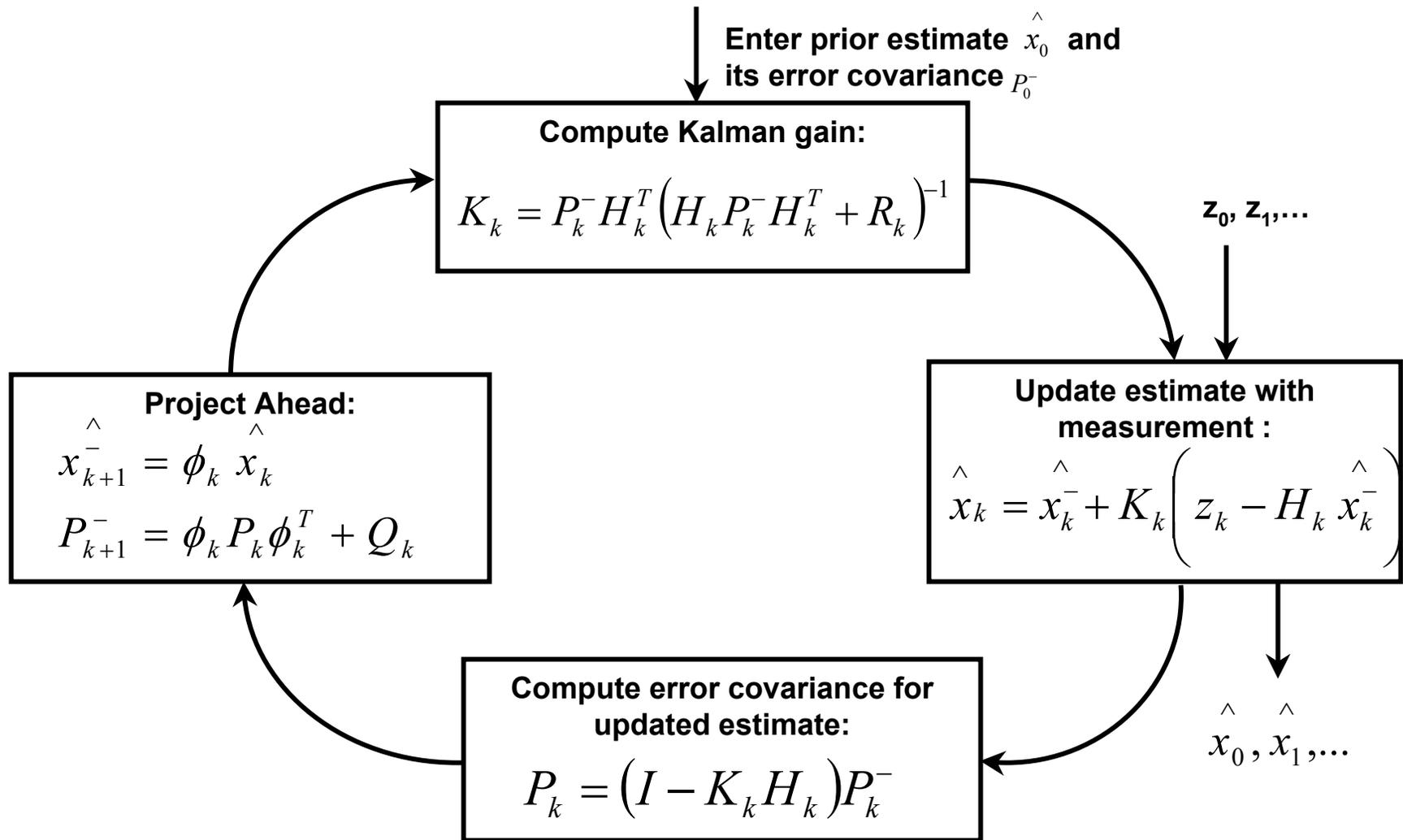
# Filtering of Absolute Disparities

Estimation of bias if it were to be present

- Ordinary Least Squares Filtering
- Kalman Filtering



# Kalman Filter Equations



Where,

$x_k$  is the process state vector at time  $t_k$

$\phi_k$  is the state transition matrix

$z_k$  is the measurement at time  $t_k$

$H_k$  is the domain transition matrix

$P_k$  is the estimation error covariance matrix

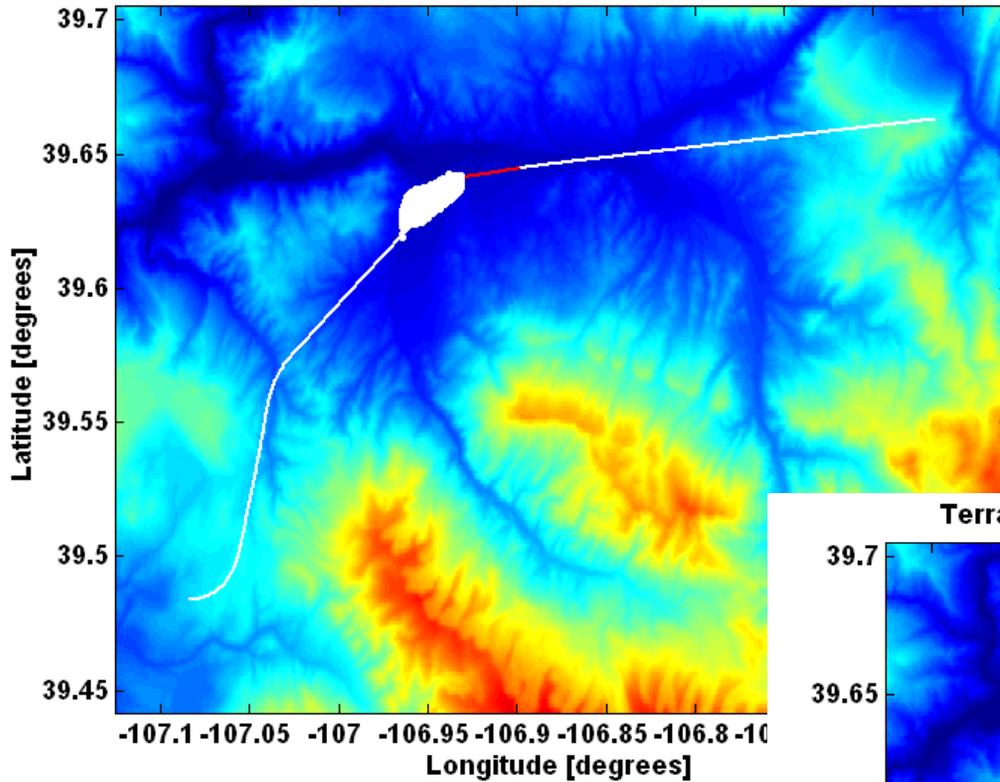
$R_k$  is the measurement error covariance matrix

$Q_k$  is the system noise covariance matrix

Kalman filtering could be used for both **terrain database integrity monitoring** and **terrain navigation**. An illustration of the former follows



Terrain Elevation & Probable Horizontal Displacement (Without Filtering)

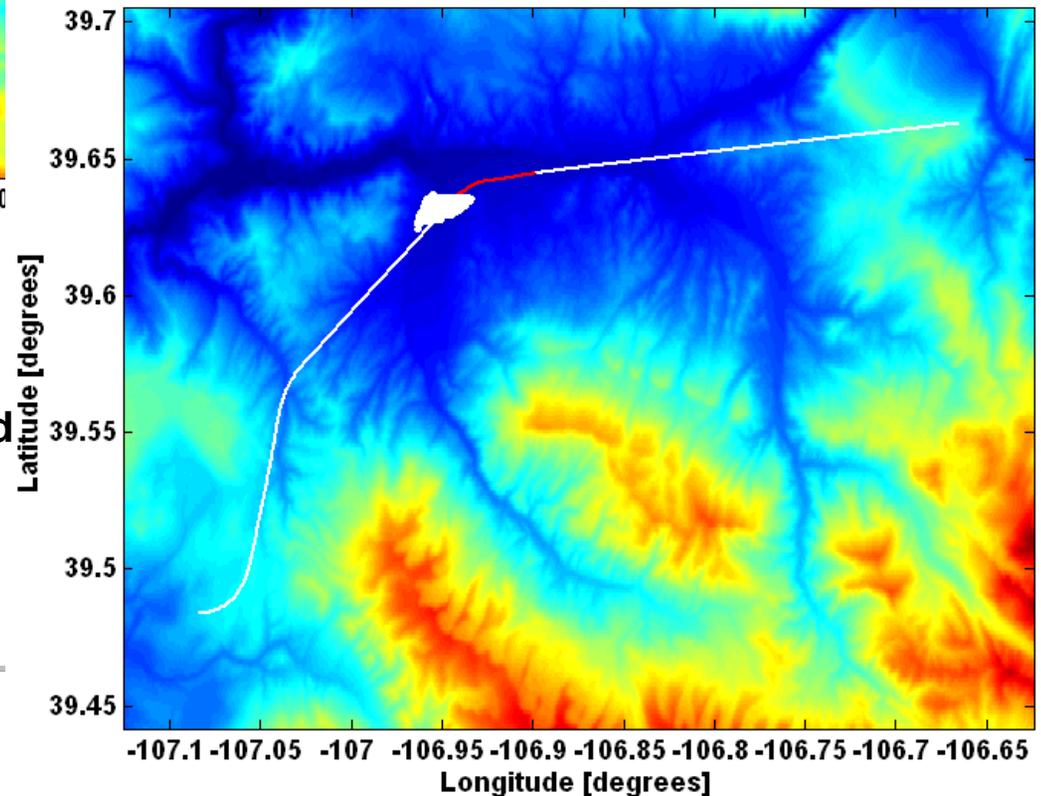


# Approach to R/W 25, EGE

Minimum T offset = 92.6 m South and 71.3 m West

Maximum Displacement = 2,124 m

Terrain Elevation & Horizontal Displacement (After Filtering)

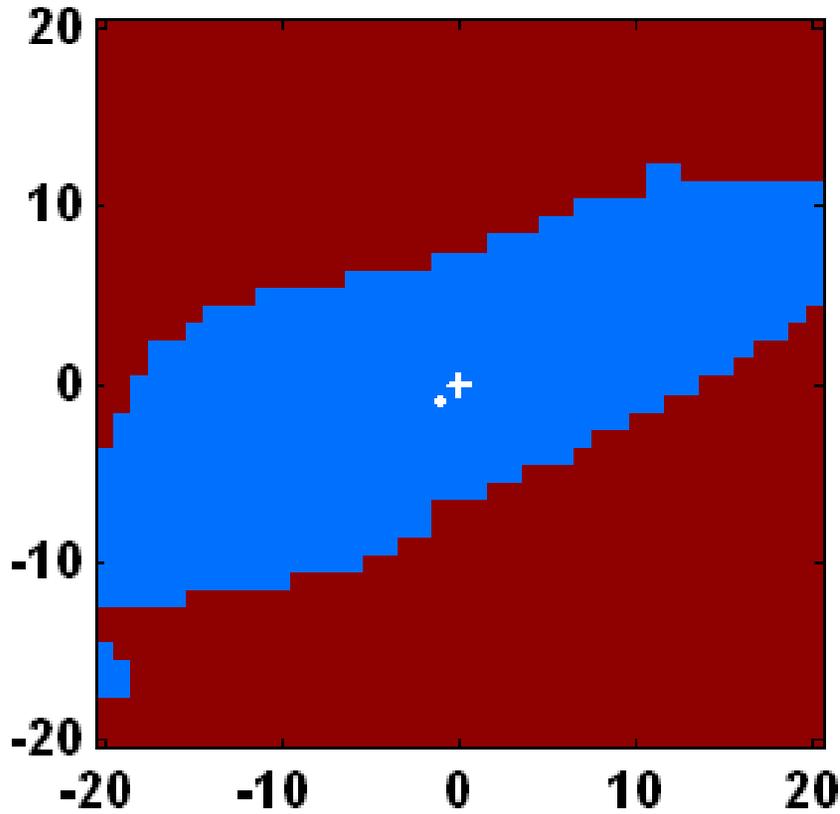


Minimum T offset = 92.6 m South and 214 m West

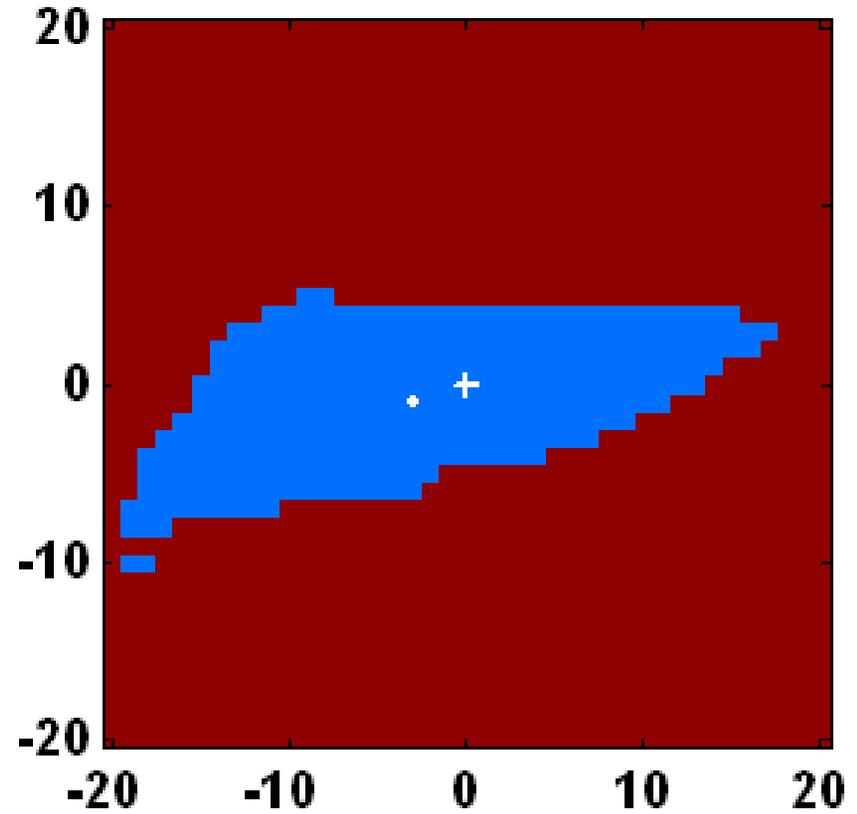
Maximum Displacement = 1,641 m

# Threshold Diagram

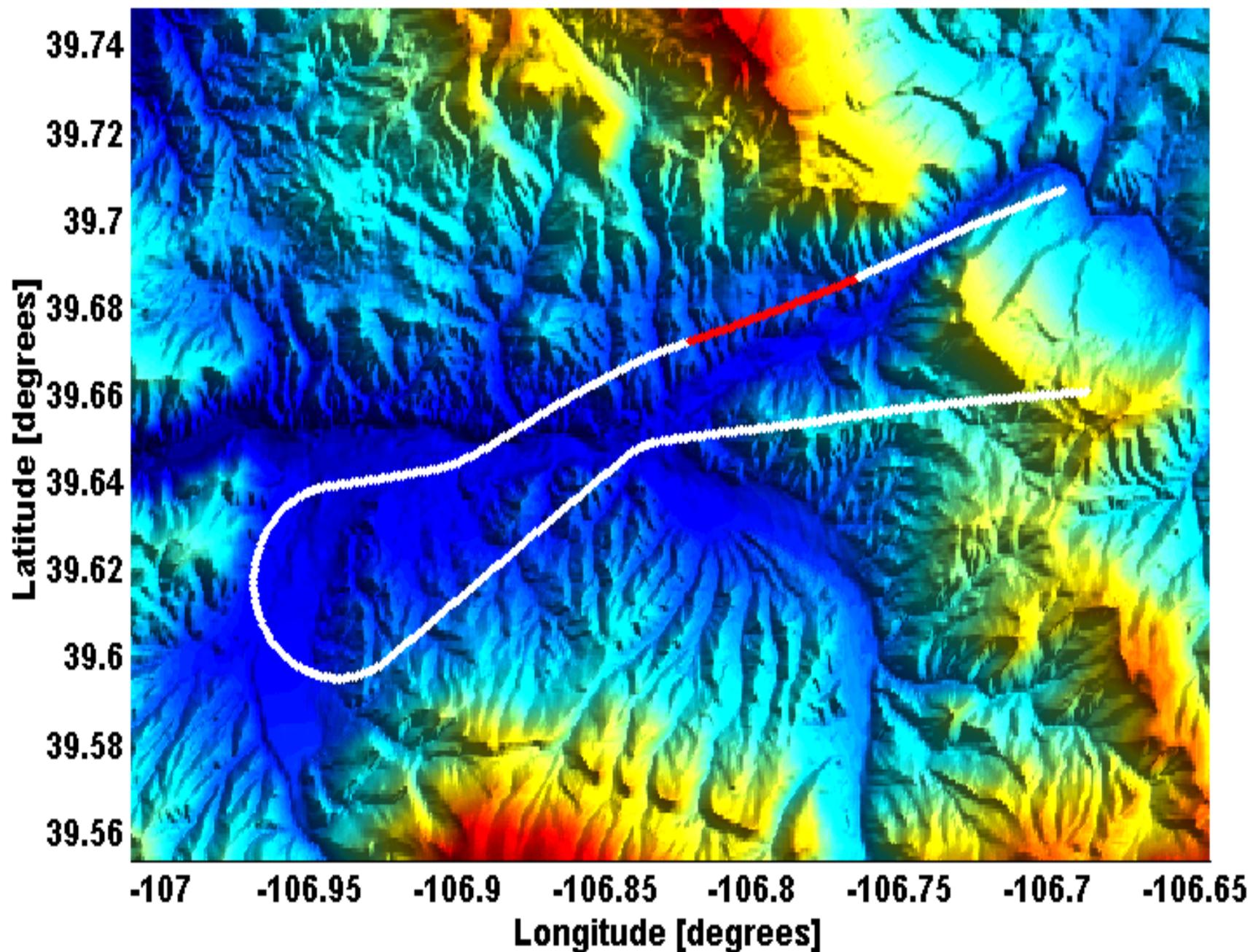
**Before Filtering**



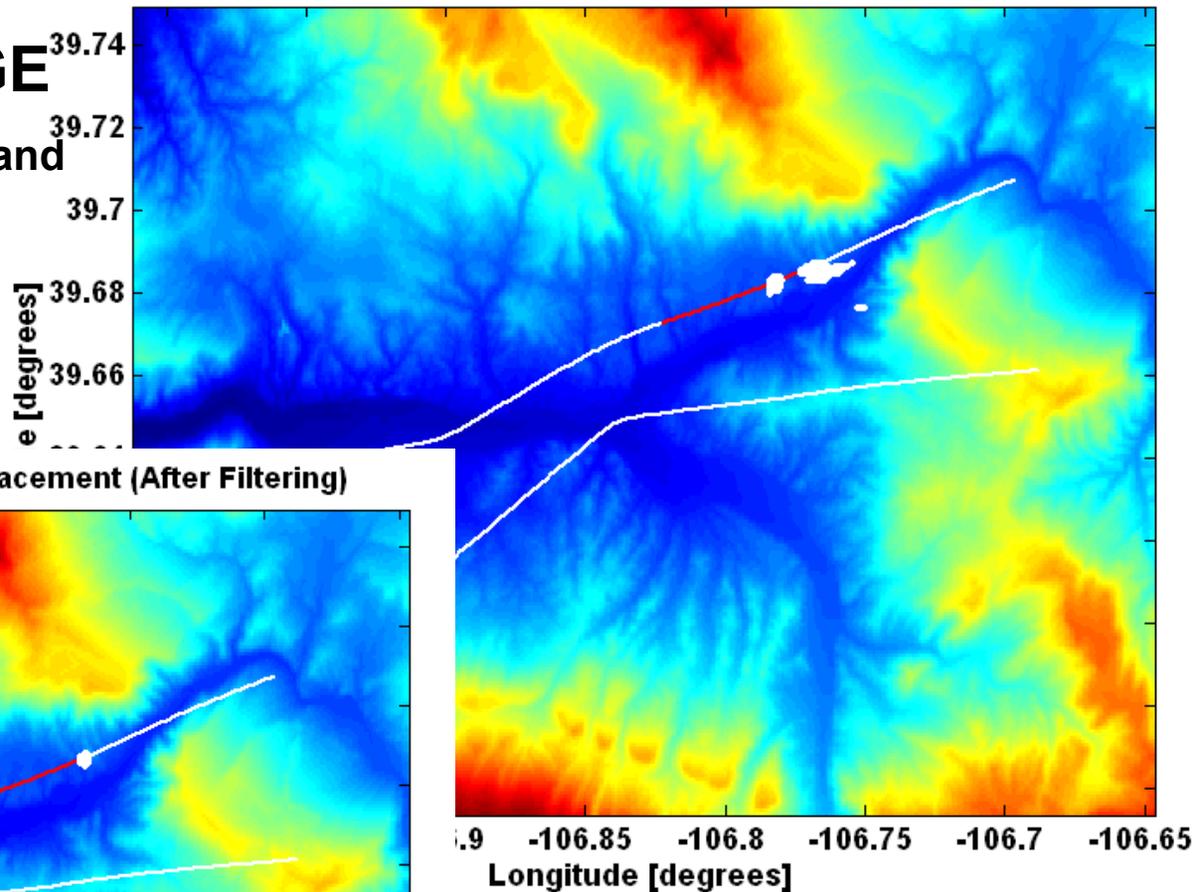
**After Filtering**



# Terrain Elevation & Flight Path Plot



Terrain Elevation & Probable Horizontal Displacement (Without Filtering)



Minimum T offset = 92.6 m South and  
142 m West

Maximum Displacement = 163 m

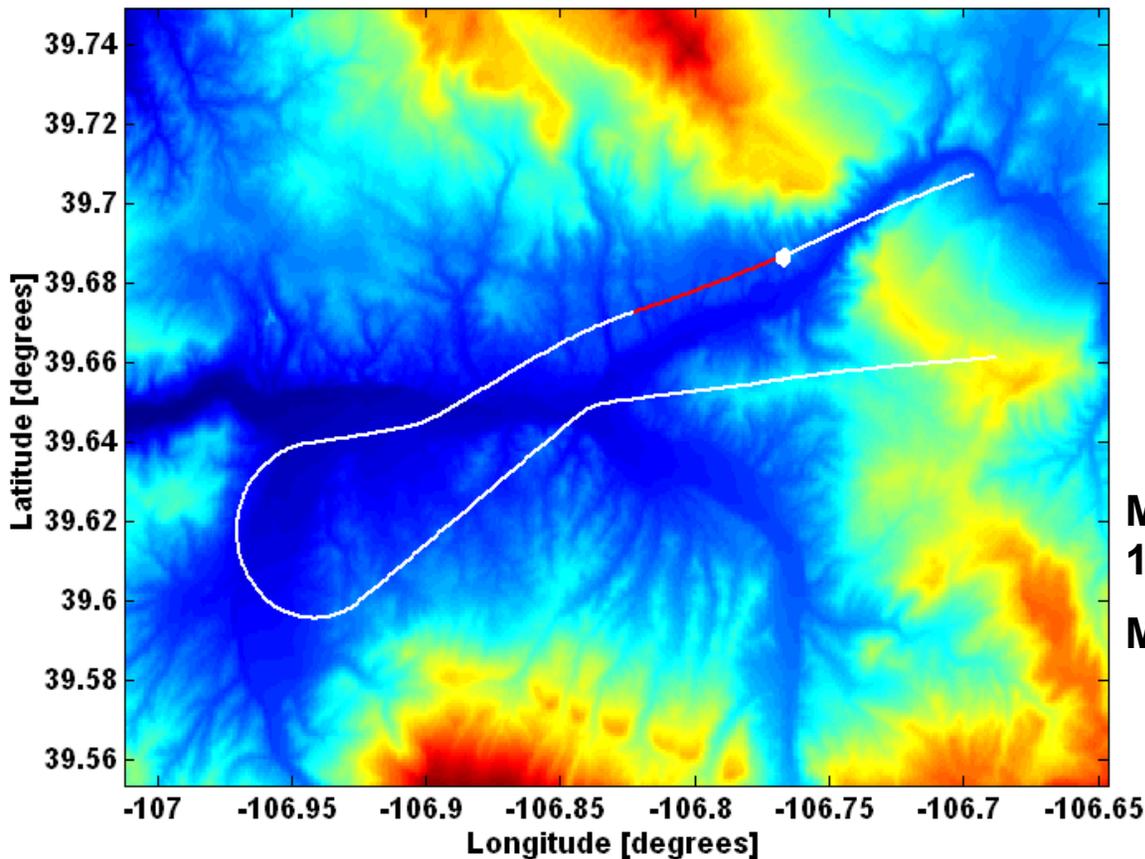


# Approach to R/W 7, EGE

Minimum T offset = 92.6 m South and  
0 m West

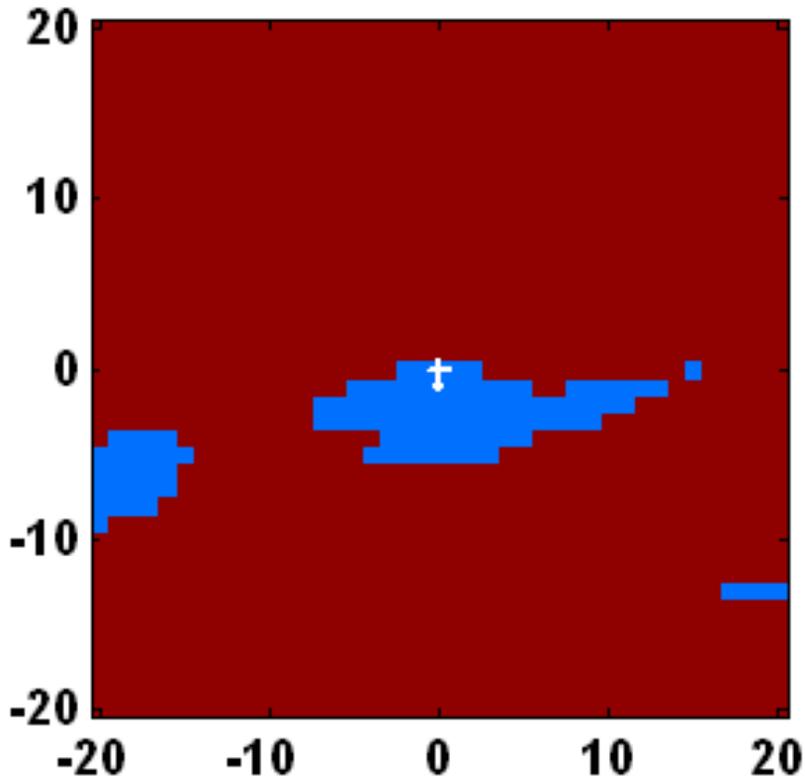
Maximum Displacement = 1,865 m

Terrain Elevation & Horizontal Displacement (After Filtering)

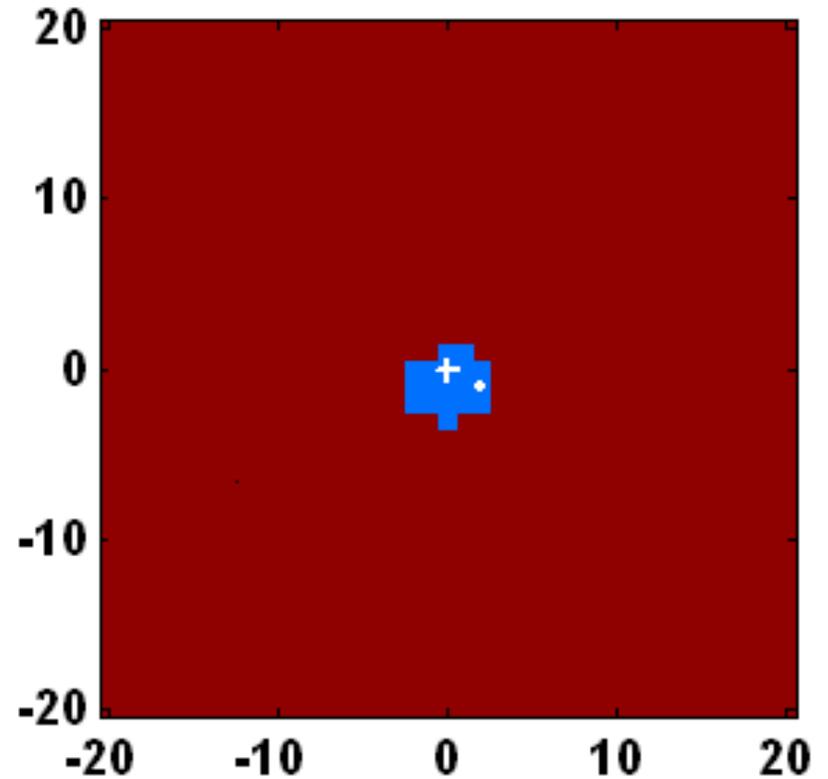


# Threshold Diagram

**Before Filtering**



**After Filtering**



# Information Content of the Terrain

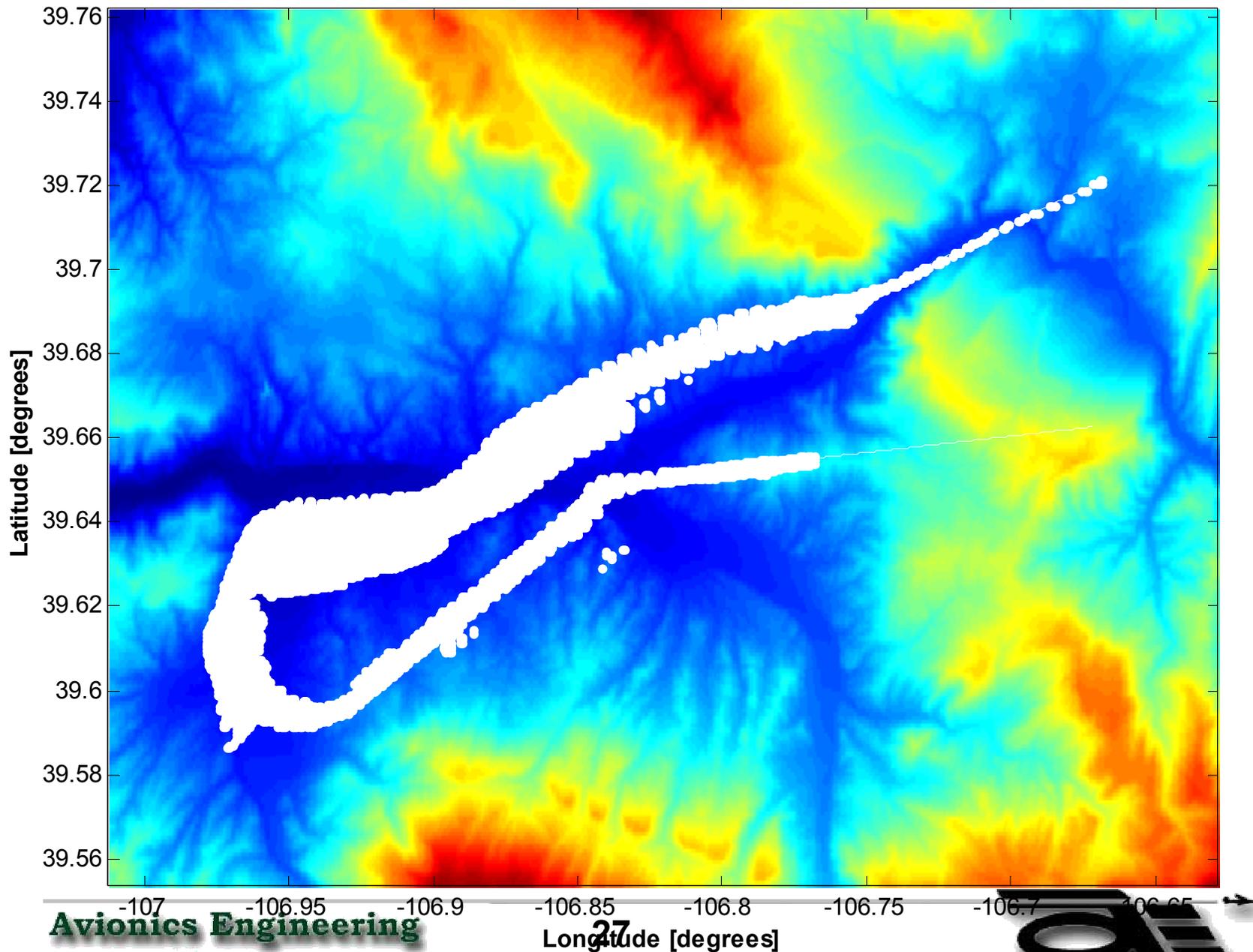
$$I = \sqrt{\frac{1}{N} \sum_{i=1}^N (\Delta h_{synth})^2}$$

$$I = \sqrt{\frac{1}{N} \sum_{i=2}^N (h_{synth}(i) - h_{synth}(i-1))^2}$$

The performance of the Horizontal Integrity Monitor directly depends upon the Terrain Signature



# Region of Missed Detection (Unfiltered)

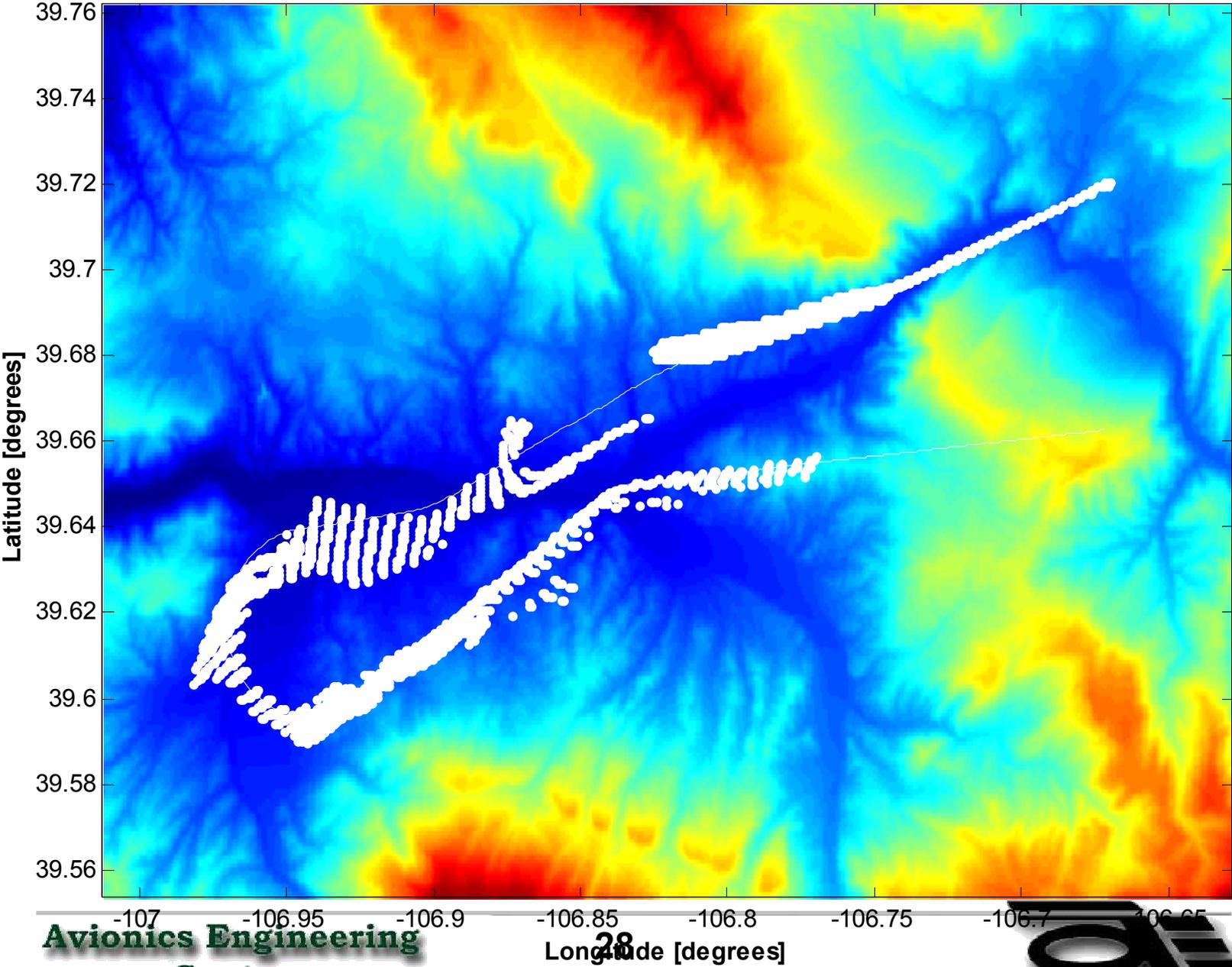


**Avionics Engineering  
Center**

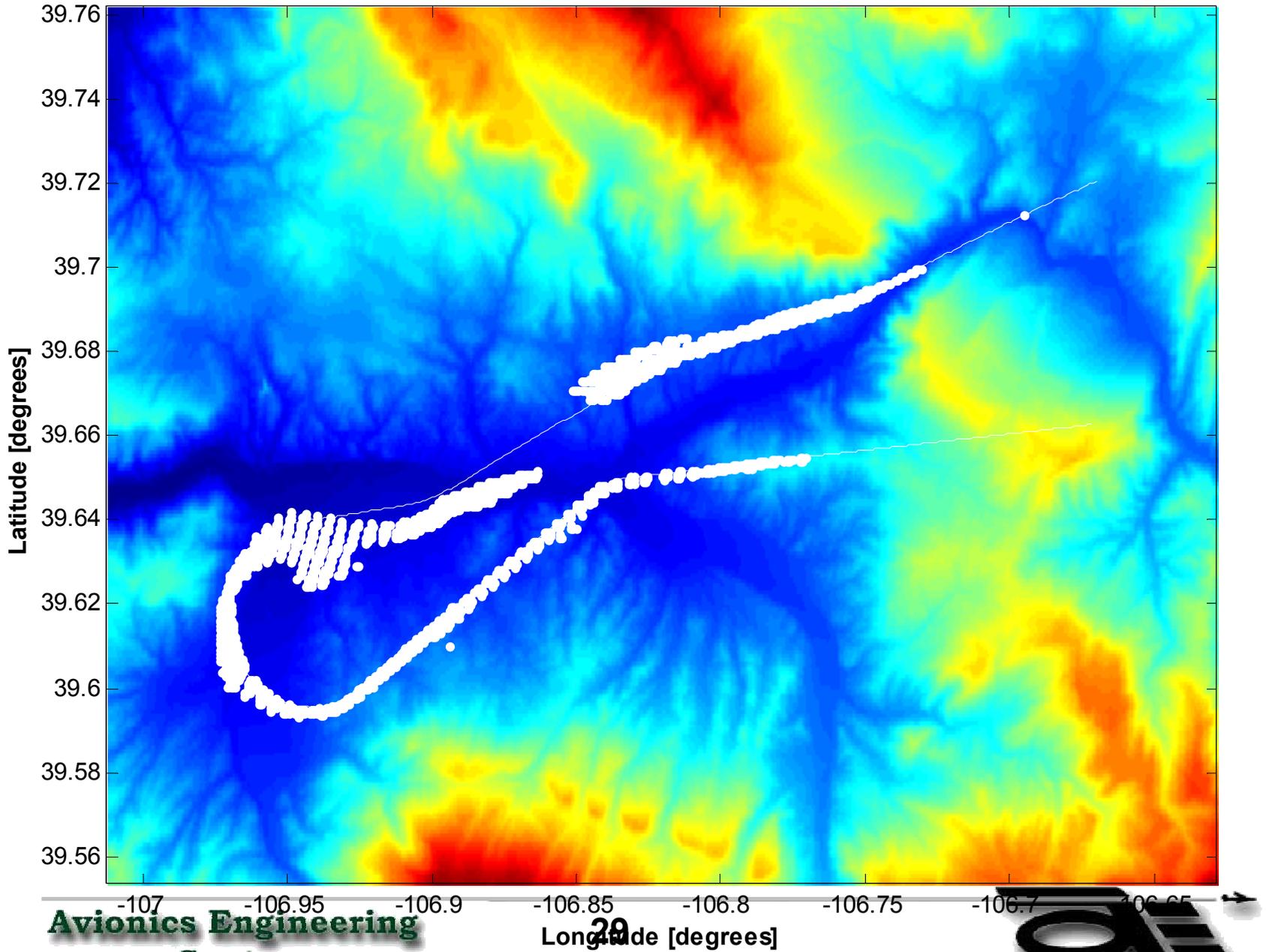
27  
Longitude [degrees]



Region of Missed Detection (LS)



# Region of Missed Detection (Kalman Covariance)

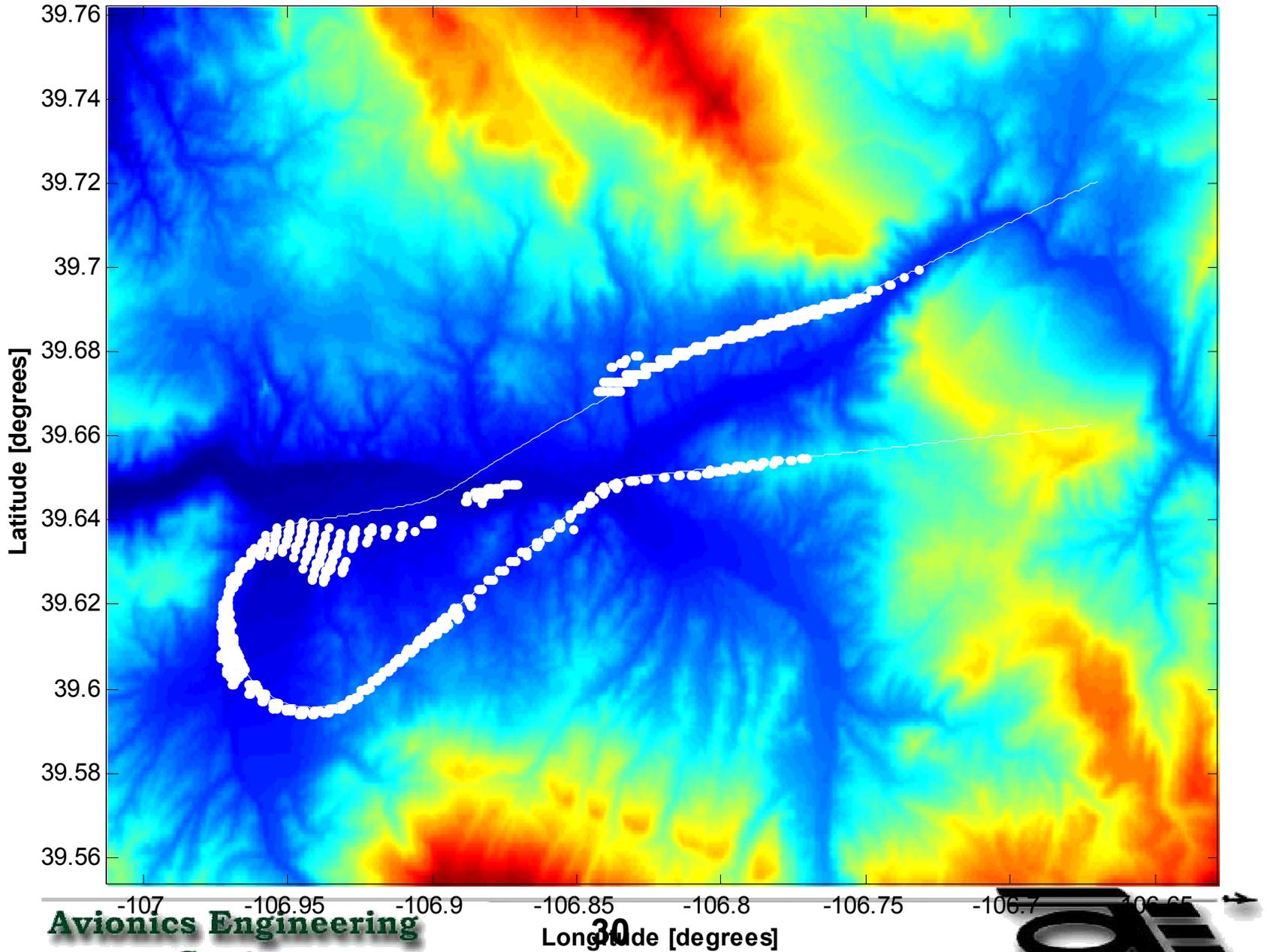


**Avionics Engineering  
Center**

Longitude [degrees]



# Region of Missed Detection (Kalman Monte Carlo)



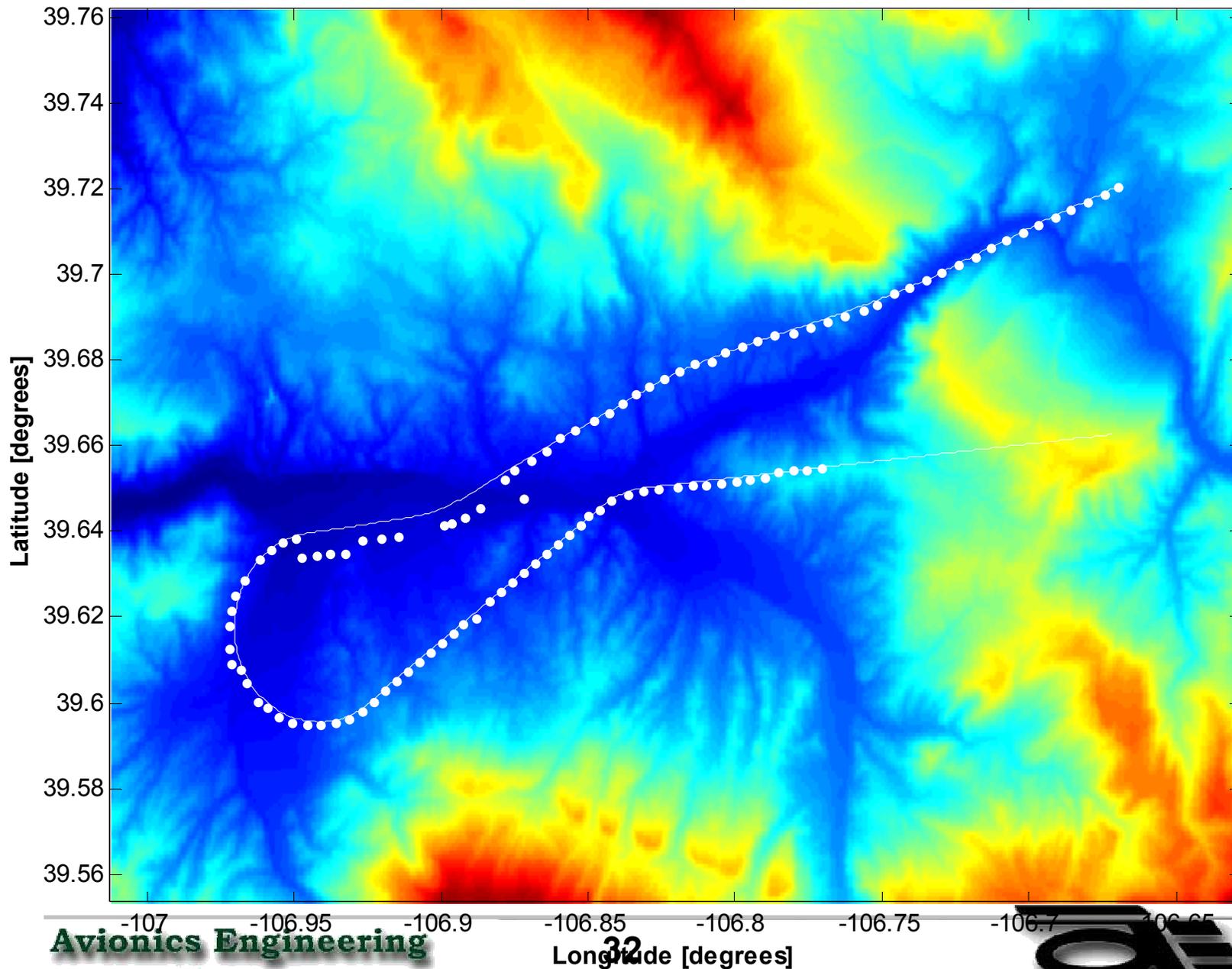
# Terrain Navigation

- The 'T' statistic can also be used for Terrain Navigation. a.k.a Map-aided Navigation
- It is a measure of the agreement of the synthesized and database terrain profiles
- Minimum T position ~ Maximum agreement

Military examples of terrain navigation: TERCOM, SITAN



# Minimum T Position (Unfiltered)

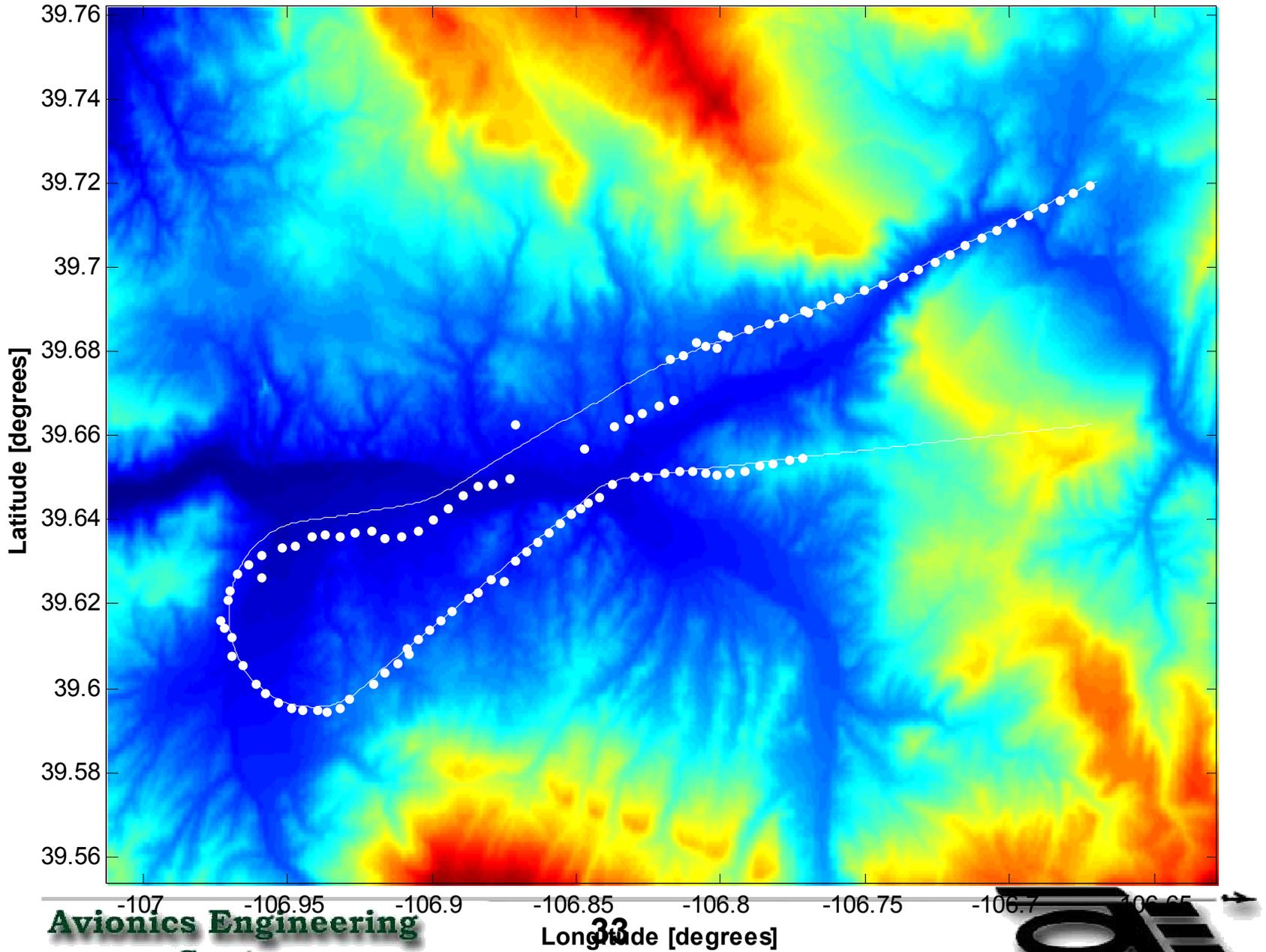


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Center**

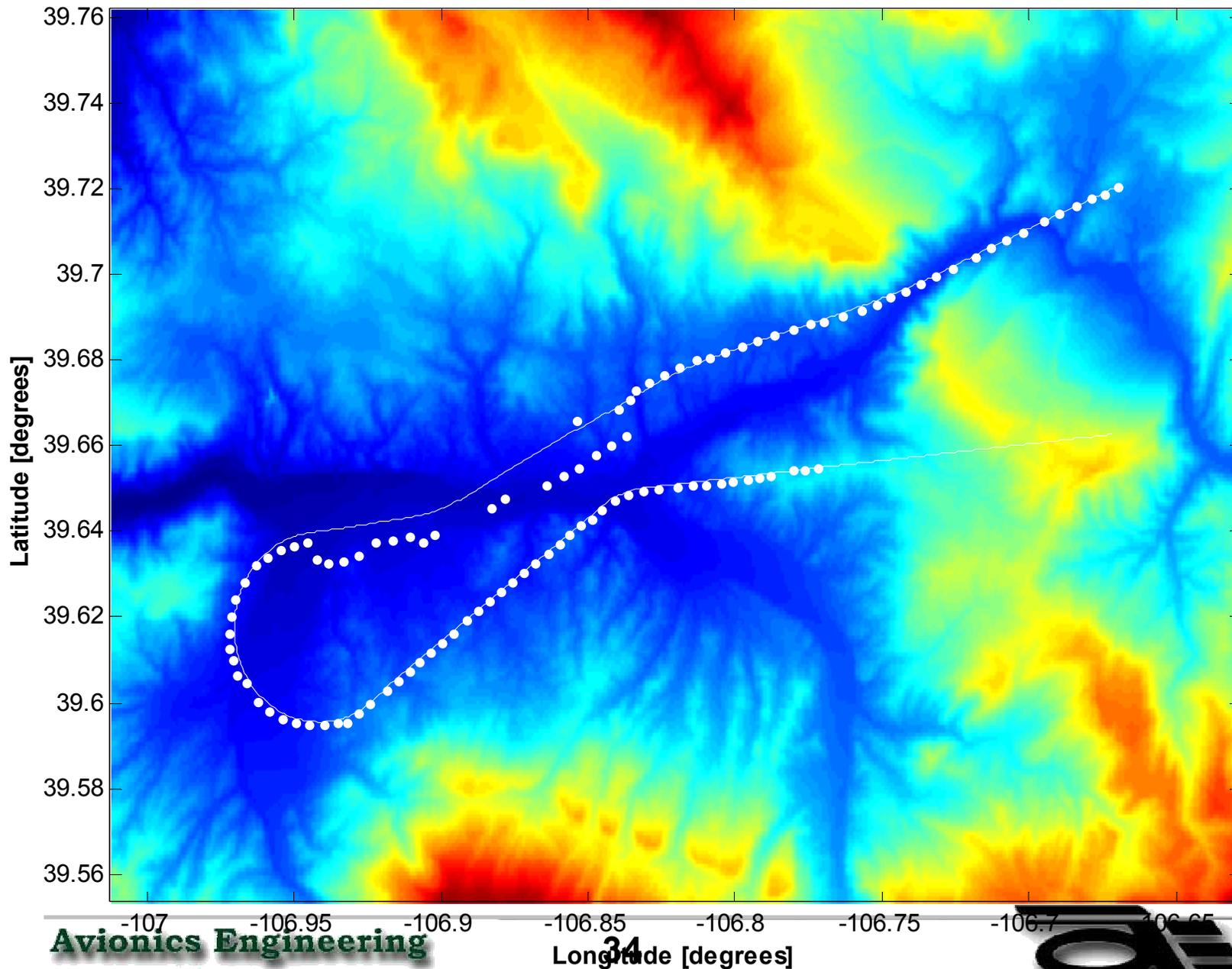
32  
Longitude [degrees]



# Minimum T Position (Least Squares)



# Minimum T Position (Kalman Covariance)

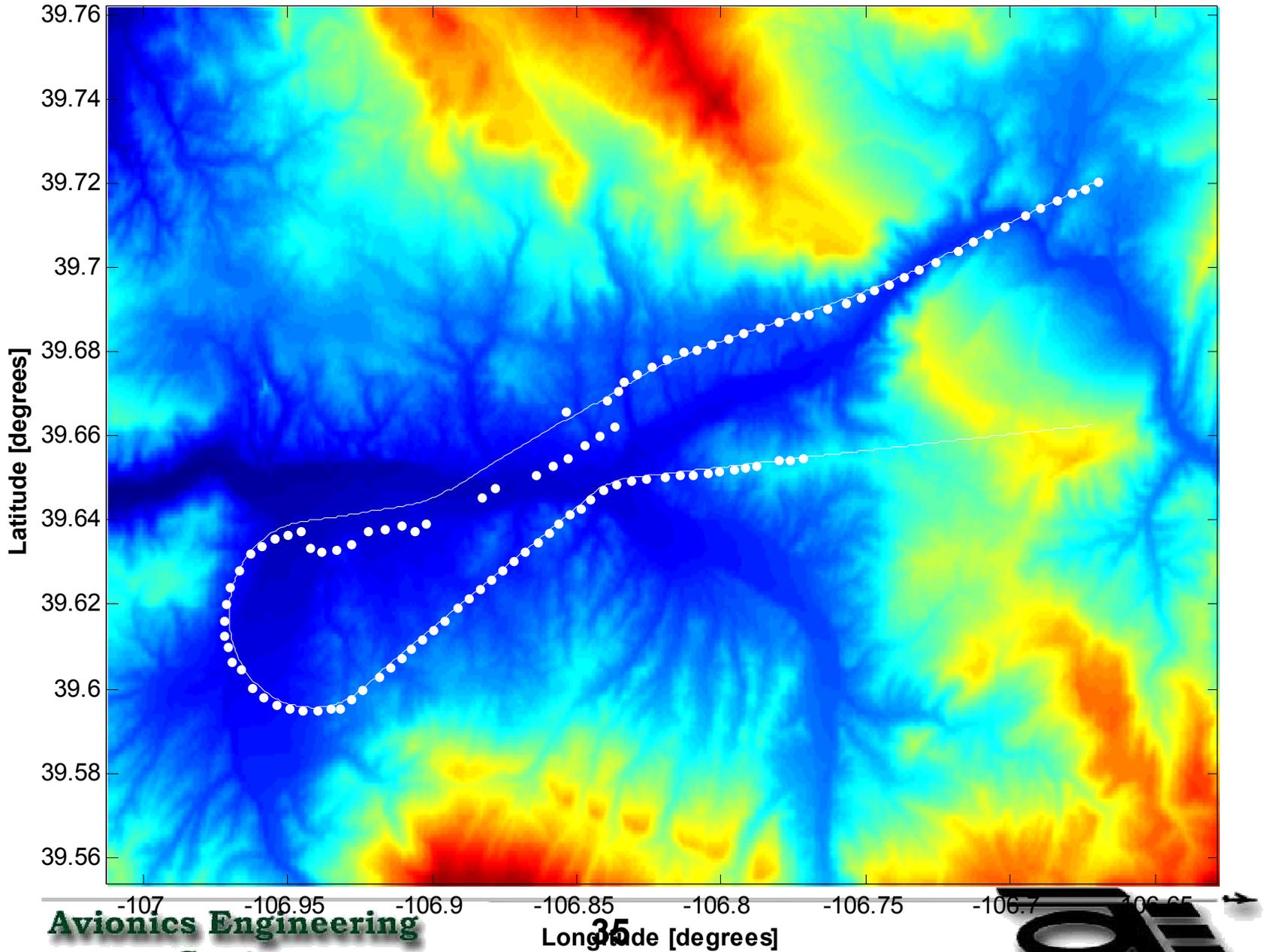


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34  
Longitude [degrees]



# Minimum T Position (Kalman Monte Carlo)

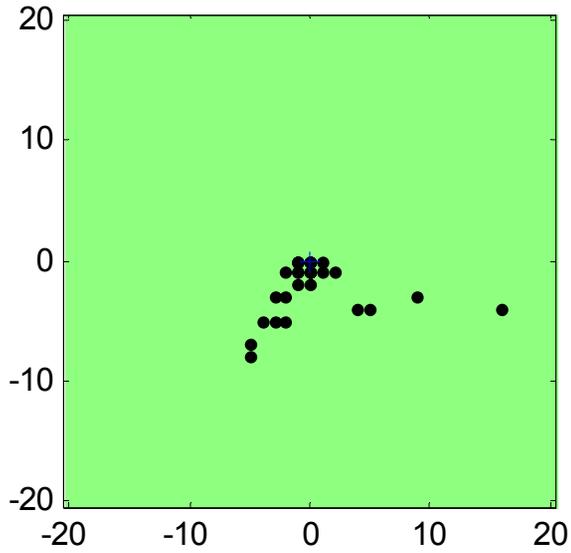


Avionics Engineering  
Center

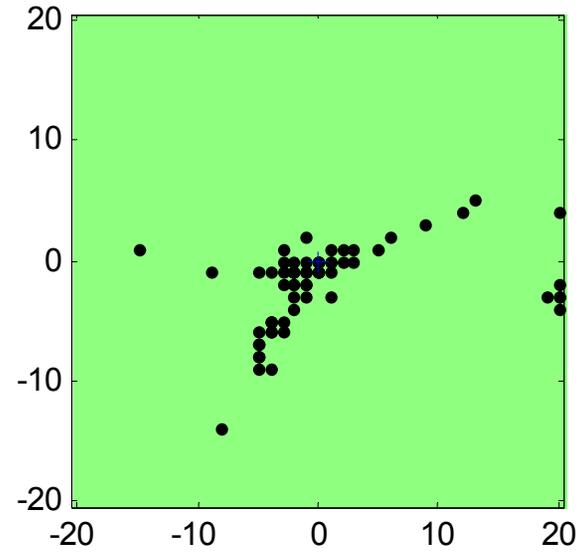
35  
Longitude [degrees]



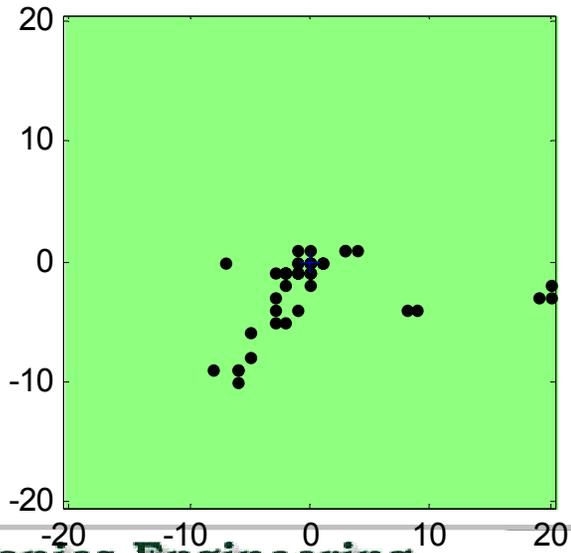
**Unfiltered**



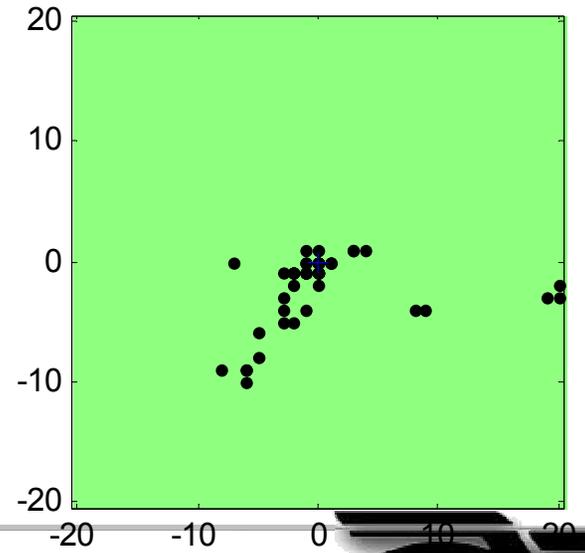
**Least Squares**



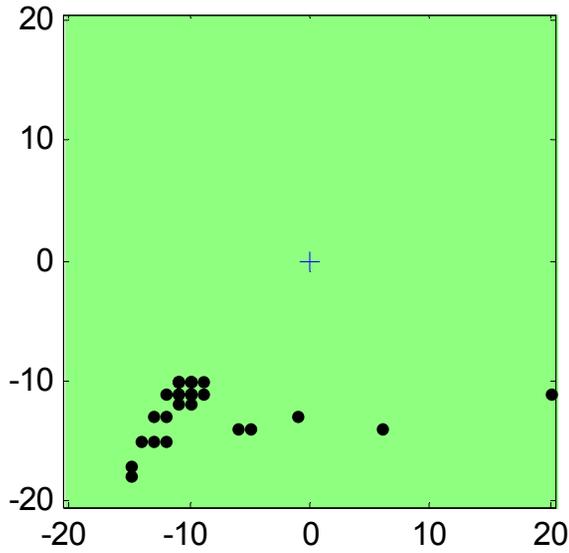
**Kalman Estimation Covariance**



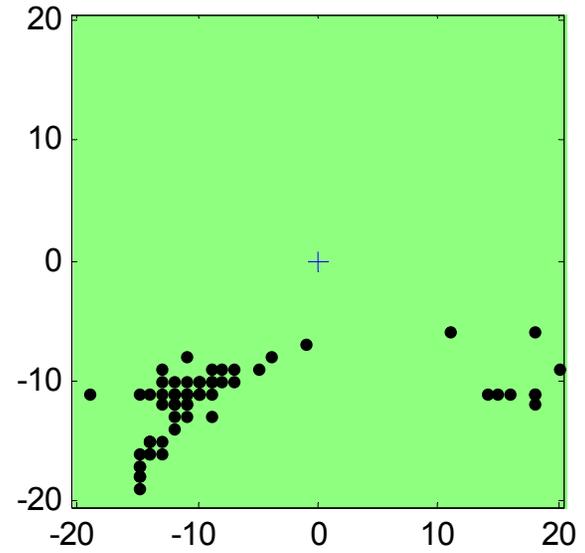
**Kalman Monte Carlo**



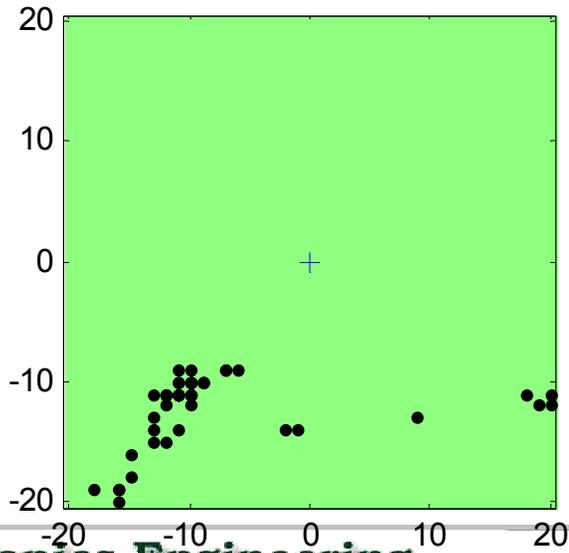
**Unfiltered**



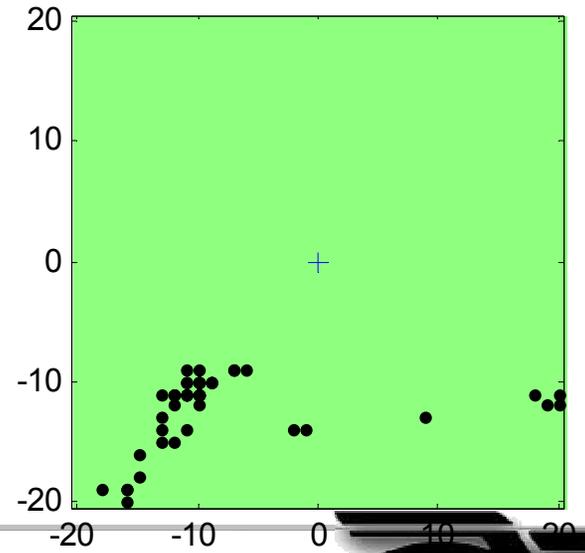
**Least Squares**



**Kalman Estimation Covariance**



**Kalman Monte Carlo**



# Conclusions and Continuing Research

- Kalman filter improves the statistical estimation capability for terrain database integrity monitoring, and its potential yet to be explored for terrain navigation
- Development of an algorithm that would perform well when the aircraft undergoes a sharp turn
- Kalman filtering could be applied in a dynamic case to reduce the noise on the sensor measurements
- The next step is to go from estimation to detection that would allow the vehicle to navigate autonomously
- The integrity monitor could help SVS to meet reliability requirements for safety critical certification levels



# References

1. Campbell, J., "Characteristics of a real-time digital terrain database integrity monitor for a synthetic vision system, MS thesis, Department of Electrical and Computer Engineering, Ohio University, Athens, Ohio, November 2001.
2. Gray, R.A., "Inflight Detection of Errors for Enhanced Aircraft Flight Safety and Vertical Accuracy Improvement using Digital Terrain Elevation Data With an Inertial Navigation System, Global Positioning System and Radar Altimeter", Ph.D. Dissertation, Department of Electrical and Computer Engineering, Ohio University, Athens, Ohio, 1999.
3. Brown, R. G and Hwang, P.Y.C., Introduction to Random Signals and Applied Kalman Filtering, John Wiley & Sons, 1997
4. Uijt de Haag, M., Campbell, J., Gray, R.A., "A Terrain Database Integrity Monitor for Synthetic Vision Systems"
5. Bergman, N., Ljung, L. and Gustafsson, F., "Terrain Navigation using Bayesian Statistics"

